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(54) Title: IMPROVED MATERIAL AND METHOD TO DISSOCIATE WATER (57) Abstract A material and method to decompose/dissociate water into hydrogen and oxygen. The material comprises a reactive alloy of an alkali metal and aluminum combined with a catalytically effective amount of an alloy comprising a metal selected from the platinum metal family and at least one metal selected from the group consisting of germanium, antimony, gallium, thallium, indium and bismuth.		

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IMPROVED MATERIAL AND METHOD TO DISSOCIATE WATER

CROSS-REFERENCE TO RELATED APPLICATIONS

This application is a continuation-in-part of Application Serial No. 902,705, entitled MATERIAL AND METHOD FOR OBTAINING HYDROGEN BY DISSOCIATION OF WATER, filed on May 4, 1978; of Application Serial No. 902,708, entitled MATERIAL AND METHOD FOR OBTAINING HYDROGEN AND OXYGEN BY DISSOCIATION OF WATER, filed on May 4, 1978; of Application Serial No. 06/068,749, entitled MATERIAL AND METHOD FOR OBTAINING HYDROGEN BY DISSOCIATION OF WATER, filed on August 23, 1979; and of an application having attorney's indicia AE-109, entitled MATERIAL AND METHOD TO DISSOCIATE WATER AT CONTROLLED RATES, filed on October 16, 1979; and is related to an application having attorney's indicia AE-106, entitled HYDROGEN GENERATING APPARATUS AND METHOD, filed on October 16, 1979; and to Application Serial No. 06/056,994, entitled FUEL SYSTEM AND METHOD, filed on July 12, 1979.

BACKGROUND OF THE INVENTION

FIELD OF INVENTION

20 This invention relates to a material for and a method of effecting the decomposition/dissociation of water into hydrogen and oxygen.

The water is reacted with a reactive alloy of sodium and aluminum to form hydrogen and a metallic hydroxide
25 denoted by the formula $\text{Na}_3\text{AL}(\text{OH})_6$. The $\text{Na}_3\text{AL}(\text{CH})_6$ is unstable at the temperature of formation in the presence of a catalyst comprising a platinum group metal or nickel and at least one element selected from the group

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consisting of germanium, antimony, gallium, thallium, indium and bismuth and breaks down to form metallic sodium and aluminum thereby releasing oxygen and hydrogen.

DESCRIPTION OF THE PRIOR ART

5 It is well known in the prior art that alkali metals react with water to form hydrogen and the stable alkali metal hydroxide. The foregoing reaction is rapid, the heat generated intense and explosion of the alkali metal and hydrogen usually occurs. The result is an unsatisfactory and dangerous method of generating hydrogen. It is also well known that metal peroxides may be used for the generation of oxygen (see U. S. Patent 3,574,561).

10 Thermochemical cycles comprising metal-metalloid combinations for the generation of both hydrogen and oxygen are disclosed in U. S. Patent 3,969,495.

15 Closed cycle processes for dissociation of water into hydrogen and oxygen are disclosed in U. S. Patents 3,821,358, 3,928,549 and 4,011,305. Combinations of various metals in multistep processes for dissociation of water are, therefore, well known; however, the simple and facile manner of producing hydrogen and oxygen utilizing a reactive alloy of alkali metal and aluminum combined with a catalytic alloy comprising a platinum group metal or nickel and at least one element selected from the group consisting of germanium, antimony, gallium, thallium, indium, and bismuth has not heretofore been appreciated.

DESCRIPTION OF THE INVENTION

20 The material I have found to be suitable for the generation of hydrogen and oxygen from water without spontaneous combustion of the resultant evolved hydrogen and oxygen gases comprise a reactive alloy of (1) an alkali metal such as lithium, sodium, potassium, cesium, or combinations thereof, and (2) aluminum combined with a catalytic alloy comprising a platinum group metal or nickel and at least one element selected from the group consisting of germanium, antimony, gallium, thallium, indium and bismuth.

The melting point of sodium and aluminum is such as to enable the formation of a liquid solution of sodium and aluminum when the two are intermixed in a liquid state above their respective melting points.

5 The atomic weight ratio of alkali metal to aluminum is from about 1:100 to about 100:1. Preferably the atomic weight ratio of alkali metal to aluminum is from about 1:3 to about 3:1.

10 The reactive alloy of alkali metal and aluminum is combined with a catalytically active alloy which is present in a catalytically effective amount and, at the conditions of hydrogen generation, functions to regenerate the reactive alloy to the reactive alloy state.

15 It is essential that the catalyst/alloy contain a platinum group metal or nickel and at least one element selected from the group consisting of germanium, antimony, gallium, thallium, indium, and bismuth.

20 Preferably the catalyst comprises platinum and at least one element selected from the group consisting of germanium, antimony, gallium, thallium, indium and bismuth.

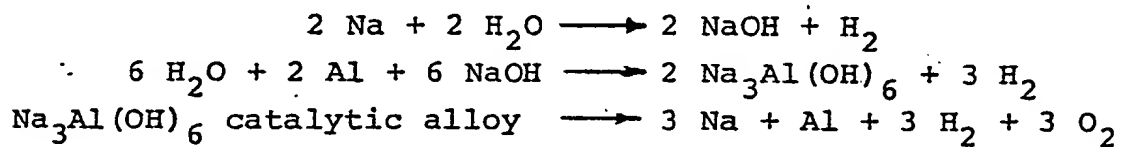
Catalytic activity is further enhanced by the addition of minor amounts of zirconium and chromium.

25 Silver, tin and/or gold may be incorporated in the catalyst as an alloying element to lower the melting point of the alloy.

30 The catalytic alloy and the reactive alloy may be compounded with an extender. The extender functions both to dilute the reactive alloy-catalytic alloy combination and to provide a heat conducting medium to dissipate the heat generated during the dissociation of water by contact with the combined reactive alloy and catalytic alloy away from the reaction zone. The extender is preferably tin although other metals which do not
35 readily oxidize in the presence of heat or water and are nonreactive with water may also function as extenders.

The combination of reactive alloy and catalytic alloy, or reactive alloy, catalytic alloy and extender is most suitable in a solid block form, regardless of size, hereinafter referred to as a reactor block.

5 Although not wishing to be bound by the following explanation, it is believed that the water reacts with the alkali metal, e.g., sodium, and the aluminum liberating hydrogen and forming $\text{Na}_3\text{Al}(\text{OH})_6$. The $\text{Na}_3\text{Al}(\text{OH})_6$ is unstable in the presence of the catalytic alloy at
10 the conditions of $\text{Na}_3\text{Al}(\text{OH})_6$ formation, and the foregoing decomposes to release the H_2 , O_2 and regenerated reactive alloy. The catalytic alloy apparently functions to catalyze the decomposition, and thereby extends the life of the reactive alloy. The process may be depicted
15 as follows:



It is preferred to include chromium as an additional
20 component of the catalytic alloy. The incorporation of chromium as a component of the catalytic alloy appears to lower the heat of reaction. The chromium is generally present in the alloy in an amount measured on a weight percent basis of said catalytic alloy of from about
25 0.7% to about 1.1% and preferably from about 0.8% to about 0.9%.

Each of the components of the catalytic alloy may be present in amounts of from about 0.4% by weight to about 28.5% by weight based on the weight of the combined
30 catalytic alloy and reactive alloy.

The preferred catalytic alloy, provided no extender is used, comprises (1) a platinum group metal or nickel present in amounts of from about 0.7 to about 1.1% by weight, (2) antimony present in an amount of from about
35 25.5 to about 42.5% by weight, (3) tin present in an amount of from about 42.9 to about 71.5% by weight,

(4) chromium present in an amount of from about 0.7 to about 1.1% by weight, (5) zirconium present in an amount of from about 4.1 to about 6.8% by weight and gold present in an amount of from about 1.1 to about 1.9% by weight.

A specific example of said preferred catalytic alloy comprises about 0.9 wt. % platinum, about 34.0 wt. % antimony, about 57.3 wt. % tin, about 0.9 wt. % chromium, about 5.4 wt. % zirconium and about 1.5 wt. % gold.

The reactive alloy of sodium and aluminum is prepared by volumetric blending in the molten state of the two metals with the proviso that both metals must be free of oxides and/or hydroxides prior to blending and that they must be kept in an inert atmosphere after blending and at all times prior to and during mixing with the catalytic alloy.

The resulting reactive alloy may be maintained in the molten state and in an inert atmosphere if it is to be blended with the catalytic alloy immediately. It may be cooled for further blending at a later time provided it is maintained in an atmosphere free of any moisture, oxygen and or nitrogen.

As in the preparation of the reactive alloy and all other steps in the method of manufacture of the various compositions of this invention, precautions must be taken during preparation to avoid the presence of oxygen, nitrogen and/or water inasmuch as these materials coming in contact with the materials before final heat stabilization tend to act as a poison to the resultant material.

The preparation of the selected catalytic alloy may be in any well known manner having in mind the proviso that an inert atmosphere be maintained whether in the molten state or as a cooled solid.

The catalytic alloy when used in the molten liquid state may be combined on a volumetric basis at the elevated temperatures required to maintain a liquid state and after said volumetric blending in the proportions

required may be cooled into a solid block or in small granules utilizing any well known manner of granulating with the proviso that the material be maintained in an inert atmosphere until it has cooled after final blending.

5 The specific manner of catalysis is not known, but generally catalysis is a surface phenomenon and consistent therewith in the instant invention it appears that the catalysis is related to both particle size and nature as well as uniformity of mixture of the reactive alloy
10 and the catalytic alloy.

 The reactive alloy and catalytic alloy may be used (1) in particulate form such as a floating bed, or other intimate dispersion, (2) in the form of a porous mass which may be formed by compression or sintering, or (3)
15 as a solid mass by alloying of the reactive alloy and the catalytic alloy. By alloying, it is meant that the reactive alloy and the catalytic alloy are combined to form an admixture or metal solution and alloyed under inert conditions at a temperature above the melting point of
20 said admixture.

 In either of the foregoing forms an extender, such as gallium, silver, titanium, magnesium, molybdenum, tungsten, nickel, rhodium, iron, palladium, cobalt, chromium, tin, iridium, lead, vanadium, gold and zircon-
25 ium may be used. The extender functions to vary activity by controlling the conductance of heat away from the reaction zone on water contact. The higher the temperature of the reaction zone on water contact the more rapid the catalysis of the unstable sodium-aluminum-hydroxide
30 to the reactive metal and hydrogen and oxygen gases.

 Admixture of the extender with the reactive alloy and the catalytic alloy is effected by utilizing the extender in the molten state and blending on a volumetric basis with the molten alloys.

EXAMPLE I

PREPARATION OF REACTIVE ALLOY

A reactive alloy comprising 35.144 parts by weight of sodium and 13.749 parts by weight of aluminum is combined volumetrically at a temperature above the melting temperature of the highest melting point element in an inert atmosphere and in the state of agitation at the volumetric blending point.

The resulting reactive alloy is maintained in the molten state and its temperature is increased to a temperature above the melting temperature of the catalytic alloy for volumetric blending with the catalytic alloy and the extender if utilized.

PREPARATION OF CATALYTIC ALLOY

0.3 parts by weight platinum, 11.3 parts by weight antimony, 19.0 parts by weight bismuth, 1.8 parts by weight zirconium, 0.3 parts by weight chromium and 0.5 parts by weight gold are introduced into a crucible which is placed in an oven and heated to melting in an inert atmosphere to form an alloy of said metals.

The resulting alloy is maintained at a temperature above its melting point for the admixing at the molten metal state with the reactive alloy. The molten alloy is maintained in an inert atmosphere throughout the process to prevent oxidation of the catalytic alloy at the elevated temperature.

FORMATION OF INTIMATE REACTIVE ALLOY
AND CATALYTIC ALLOY SOLUTION

One and one-half parts by weight of reactive alloy is blended volumetrically with one part by weight of catalytic alloy in the molten liquid state said blending being carried out in an inert atmosphere.

After blending to provide a uniform solution of alloys, the resultant mixture may be cooled under the inert atmosphere in a suitable mold or other form adaptable for end use application.

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FORMATION OF REACTOR BLOCK COMPRISING
REACTIVE ALLOY, CATALYTIC ALLOY AND
EXTENDER

5 The liquid reactive alloy and liquid catalytic alloy prepared above and a liquid extender are admixed in the following proportions:

21.293 parts by weight reactive alloy.

14.062 parts by weight catalytic alloy.

64.645 parts by weight tin.

10 The blending of the foregoing metallic compounds should be done in an inert atmosphere.

After blending, the resultant mixture is poured into a suitable mold conforming to a desired shape under an inert atmosphere and allowed to solidify under the inert
15 atmosphere.

The entire foregoing procedure should be carried out under an inert atmosphere such as helium or argon and in the absence of contaminants. Oxidation of the metallic components and/or hydroxide formation will "poison" the
20 resulting reactor block and reduce the activity thereof. Moreover, during the steps of the process operated at elevated temperature, the presence of any oxygen will cause the mass to ignite.

The reactor blocks are contacted with a fine spray
25 of water at about room temperature in an atmospheric environment. The gaseous effluent from said contact comprises hydrogen and oxygen and burns when subjected to electrical sparking. The volume of gas evolved is dependent on reactor block surface area and the volume of
30 water impinging thereon. Generally a 2.5 square cm surface will react with 0.14 gallons of water per minute.

EXAMPLE II

PREPARATION OF REACTIVE ALLOY

A reactive alloy comprising 32.112 parts by weight of potassium and 37.688 parts by weight of aluminum is combined volumetrically at a temperature above the melting temperature of the highest melting point element in an inert atmosphere and in the state of agitation at the volumetric blending point.

The resulting reactive alloy is maintained in the molten state and its temperature is increased to a temperature above the melting temperature of the catalytic alloy for volumetric blending with the catalytic alloy and the extender if utilized.

PREPARATION OF CATALYTIC ALLOY

60.7 parts by weight bismuth, 0.8 parts by weight platinum, and 38.5 parts by weight germanium are introduced into a crucible which is placed in an oven and heated to melting in an inert atmosphere to form an alloy of said metals.

The resulting alloy is maintained at a temperature above its melting point for the admixing at the molten metal state with the reactive alloy. The molten alloy is maintained in an inert atmosphere throughout the process to prevent oxidation of the catalytic alloy at the elevated temperature.

FORMATION OF INTIMATE REACTIVE ALLOY
AND CATALYTIC ALLOY SOLUTION

One and one-half parts by weight of reactive alloy is blended volumetrically with one part by weight of catalytic alloy in the molten liquid state said blending being carried out in an inert atmosphere.

After blending to provide a uniform solution of alloys, the resultant mixture may be cooled under the inert atmosphere in a suitable mold or other form adaptable for end use application.

FORMATION OF REACTOR BLOCK COMPRISING
REACTIVE ALLOY, CATALYTIC ALLOY AND
EXTENDER

The liquid reactive alloy and liquid catalytic alloy
5 prepared above and a liquid extender are admixed in the
following proportions:

30.400 parts by weight reactive alloy.

20.079 parts by weight catalytic alloy.

49.522 parts by weight tin.

10 The blending of the foregoing metallic compounds
should be done in an inert atmosphere.

After blending, the resultant mixture is poured into
a suitable mold conforming to a desired shape under an
inert atmosphere and allowed to solidify under the inert
15 atmosphere.

The entire foregoing procedure should be carried out
under an inert atmosphere such as helium or argon and in
the absence of contaminants. Oxidation of the metallic
components and/or hydroxide formation will "poison" the
20 resulting reactor block and reduce the activity thereof.
Moreover, during the steps of the process operated at
elevated temperature, the presence of any oxygen will
cause the mass to ignite.

The reactor blocks are contacted with a fine spray
25 of water at about room temperature in an atmospheric en-
vironment. The gaseous effluent from said contact com-
prises hydrogen and oxygen and burns when subjected to
electrical sparking. The volume of gas evolved is de-
pendent on reactor block surface area and the volume of
30 water impinging thereon. Generally a 2.5 square cm sur-
face will react with 0.28 gallons of water per minute.

EXAMPLE III

PREPARATION OF REACTIVE ALLOY

A reactive alloy comprising 32.112 parts by weight of sodium and 37.688 parts by weight of aluminum is combined volumetrically at a temperature above the melting temperature of the highest melting point element in an inert atmosphere and in the state of agitation at the volumetric blending point.

The resulting reactive alloy is maintained in the molten state and its temperature is increased to a temperature above the melting temperature of the catalytic alloy for volumetric blending with the catalytic alloy and the extender if utilized.

PREPARATION OF CATALYTIC ALLOY

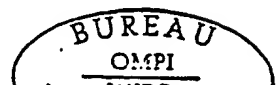
60.7 parts by weight bismuth, 0.5 parts by weight ruthenium and 38.5 parts by weight germanium are introduced into a crucible which is placed in an oven and heated to melting in an inert atmosphere to form an alloy of said metals.

The resulting alloy is maintained at a temperature above its melting point for the admixing at the molten metal state with the reactive alloy. The molten alloy is maintained in an inert atmosphere throughout the process to prevent oxidation of the catalytic alloy at the elevated temperature.

FORMATION OF INTIMATE REACTIVE ALLOY
AND CATALYTIC ALLOY SOLUTION

One and one-half parts by weight of reactive alloy is blended volumetrically with one part by weight of catalytic alloy in the molten liquid state said blending being carried out in an inert atmosphere.

After blending to provide a uniform solution of alloys, the resultant mixture may be cooled under the inert atmosphere in a suitable mold or other form adaptable for end use application.



FORMATION OF REACTOR BLOCK COMPRISING
REACTIVE ALLOY, CATALYTIC ALLOY AND
.....
EXTENDER

5 The liquid reactive alloy and liquid catalytic alloy prepared above and a liquid extender are admixed in the following proportions:

30.398 parts by weight reactive alloy.
20.138 parts by weight catalytic alloy.
49.464 parts by weight tin.

10 The blending of the foregoing metallic compounds should be done in an inert atmosphere.

After blending, the resultant mixture is poured into a suitable mold conforming to a desired shape under an inert atmosphere and allowed to solidify under the inert
15 atmosphere.

The entire foregoing procedure should be carried out under an inert atmosphere such as helium or argon and in the absence of contaminants. Oxidation of the metallic components and/or hydroxide formation will "poison" the
20 resulting reactor block and reduce the activity thereof. Moreover, during the steps of the process operated at elevated temperature, the presence of any oxygen will cause the mass to ignite.

The reactor blocks are contacted with a fine spray
25 of water at about room temperature in an atmospheric environment. The gaseous effluent from said contact comprises hydrogen and oxygen and burns when subjected to electrical sparking. The volume of gas evolved is dependent on reactor block surface area and the volume of
30 water impinging thereon. Generally a 2.5 square cm surface will react with 0.17 gallons of water per minute.

EXAMPLE IV

PREPARATION OF REACTIVE ALLOY

A reactive alloy comprising 18.391 parts by weight of sodium and 22.947 parts by weight of aluminum is combined volumetrically at a temperature above the melting temperature of the highest melting point element in an inert atmosphere and in the state of agitation at the volumetric blending point.

The resulting reactive alloy is maintained in the molten state and its temperature is increased to a temperature above the melting temperature of the catalytic alloy for volumetric blending with the catalytic alloy and the extender if utilized.

PREPARATION OF CATALYTIC ALLOY

63.064 parts by weight bismuth, 0.951 parts by weight osmium, 36.036 parts by weight antimony and 0.45 parts by weight germanium are introduced into a crucible which is placed in an oven and heated to melting in an inert atmosphere to form an alloy of said metals.

The resulting alloy is maintained at a temperature above its melting point for the admixing at the molten metal state with the reactive alloy. The molten alloy is maintained in an inert atmosphere throughout the process to prevent oxidation of the catalytic alloy at the elevated temperature.

FORMATION OF INTIMATE REACTIVE ALLOY
AND CATALYTIC ALLOY SOLUTION

One and one-half parts by weight of reactive alloy is blended volumetrically with one part by weight of catalytic alloy in the molten liquid state said blending being carried out in an inert atmosphere.

After blending to provide a uniform solution of alloys, the resultant mixture may be cooled under the inert atmosphere in a suitable mold or other form adaptable for end use application.

FORMATION OF REACTOR BLOCK COMPRISING
REACTIVE ALLOY, CATALYTIC ALLOY AND
EXTENDER

The liquid reactive alloy and liquid catalytic alloy
5 prepared above and a liquid extender are admixed in the
following proportions:

18.003 parts by weight reactive alloy.
11.950 parts by weight catalytic alloy.
70.047 parts by weight 50 wt. % tin and
10 50 wt. % bismuth.

The blending of the foregoing metallic compounds
should be done in an inert atmosphere.

After blending, the resultant mixture is poured into
a suitable mold conforming to a desired shape under an
15 inert atmosphere and allowed to solidify under the inert
atmosphere.

The entire foregoing procedure should be carried out
under an inert atmosphere such as helium or argon and in
the absence of contaminants. Oxidation of the metallic
20 components and/or hydroxide formation will "poison" the
resulting reactor block and reduce the activity thereof.
Moreover, during the steps of the process operated at
elevated temperature, the presence of any oxygen will
cause the mass to ignite.

25 The reactor blocks are contacted with a fine spray
of water at about room temperature in an atmospheric en-
vironment. The gaseous effluent from said contact com-
prises hydrogen and oxygen and burns when subjected to
electrical sparking. The volume of gas evolved is de-
30 pendent on reactor block surface area and the volume of
water impinging thereon. Generally a 2.5 square cm sur-
face will react with 0.21 gallons of water per minute.

EXAMPLE V

PREPARATION OF REACTIVE ALLOY

A reactive alloy comprising 32.112 parts by weight of cesium and 37.688 parts by weight of aluminum is combined volumetrically at a temperature above the melting temperature of the highest melting point element in an inert atmosphere and in the state of agitation at the volumetric blending point.

The resulting reactive alloy is maintained in the molten state and its temperature is increased to a temperature above the melting temperature of the catalytic alloy for volumetric blending with the catalytic alloy and the extender if utilized.

PREPARATION OF CATALYTIC ALLOY

60.7 parts by weight bismuth, 0.896 parts by weight palladium and 38.5 parts by weight germanium are introduced into a crucible which is placed in an oven and heated to melting in an inert atmosphere to form an alloy of said metals.

The resulting alloy is maintained at a temperature above its melting point for the admixing at the molten metal state with the reactive alloy. The molten alloy is maintained in an inert atmosphere throughout the process to prevent oxidation of the catalytic alloy at the elevated temperature.

FORMATION OF INTIMATE REACTIVE ALLOY
AND CATALYTIC ALLOY SOLUTION

One and one-half parts by weight of reactive alloy is blended volumetrically with one part by weight of catalytic alloy in the molten liquid state said blending being carried out in an inert atmosphere.

After blending to provide a uniform solution of alloys, the resultant mixture may be cooled under the inert atmosphere in a suitable mold or other form adaptable for end use application.

FORMATION OF REACTOR BLOCK COMPRISING
REACTIVE ALLOY, CATALYTIC ALLOY AND
.....
EXTENDER

The liquid reactive alloy and liquid catalytic alloy
5 prepared above and a liquid extender are admixed in the
following proportions:

30.398 parts by weight reactive alloy.

20.096 parts by weight catalytic alloy.

49.506 parts by weight tin.

10 The blending of the foregoing metallic compounds
should be done in an inert atmosphere.

After blending, the resultant mixture is poured into
a suitable mold conforming to a desired shape under an
inert atmosphere and allowed to solidify under the inert
15 atmosphere.

The entire foregoing procedure should be carried out
under an inert atmosphere such as helium or argon and in
the absence of contaminants. Oxidation of the metallic
components and/or hydroxide formation will "poison" the
20 resulting reactor block and reduce the activity thereof.
Moreover, during the steps of the process operated at
elevated temperature, the presence of any oxygen will
cause the mass to ignite.

The reactor blocks are contacted with a fine spray
25 of water at about room temperature in an atmospheric en-
vironment. The gaseous effluent from said contact com-
prises hydrogen and oxygen and burns when subjected to
electrical sparking. The volume of gas evolved is de-
pendent on reactor block surface area and the volume of
30 water impinging thereon. Generally a 2.5 square cm sur-
face will react with 0.31 gallons of water per minute.

EXAMPLE VI

PREPARATION OF REACTIVE ALLOY

A reactive alloy comprising 35.144 parts by weight of sodium and 13.749 parts by weight of aluminum is combined volumetrically at a temperature above the melting temperature of the highest melting point element in an inert atmosphere and in the state of agitation at the volumetric blending point.

The resulting reactive alloy is maintained in the molten state and its temperature is increased to a temperature above the melting temperature of the catalytic alloy for volumetric blending with the catalytic alloy and the extender if utilized.

PREPARATION OF CATALYTIC ALLOY

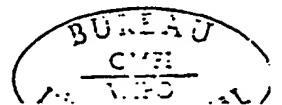
53.7 parts by weight bismuth, 34.0 parts by weight antimony, 4.5 parts by weight nickel, 1.5 parts by weight gold, 5.4 parts by weight zirconium and 0.9 parts by weight chromium are introduced into a crucible which is placed in an oven and heated to melting in an inert atmosphere to form an alloy of said metals.

The resulting alloy is maintained at a temperature above its melting point for the admixing at the molten metal state with the reactive alloy. The molten alloy is maintained in an inert atmosphere throughout the process to prevent oxidation of the catalytic alloy at the elevated temperature.

FORMATION OF INTIMATE REACTIVE ALLOY
AND CATALYTIC ALLOY SOLUTION

One and one-half parts by weight of reactive alloy is blended volumetrically with one part by weight of catalytic alloy in the molten liquid state said blending being carried out in an inert atmosphere.

After blending to provide a uniform solution of alloys, the resultant mixture may be cooled under the inert atmosphere in a suitable mold or other form adaptable for end use application.



FORMATION OF REACTOR BLOCK COMPRISING
REACTIVE ALLOY, CATALYTIC ALLOY AND
EXTENDER

The liquid reactive alloy and liquid catalytic alloy
5 prepared above and a liquid extender are admixed in the
following proportions:

21.293 parts by weight reactive alloy.

14.064 parts by weight catalytic alloy.

64.643 parts by weight gallium

10 The blending of the foregoing metallic compounds
should be done in an inert atmosphere.

After blending, the resultant mixture is poured into
a suitable mold conforming to a desired shape under an
inert atmosphere and allowed to solidify under the inert
15 atmosphere.

The entire foregoing procedure should be carried out
under an inert atmosphere such as helium or argon and in
the absence of contaminants. Oxidation of the metallic
components and/or hydroxide formation will "poison" the
20 resulting reactor block and reduce the activity thereof.
Moreover, during the steps of the process operated at
elevated temperature, the presence of any oxygen will
cause the mass to ignite.

The reactor blocks are contacted with a fine spray
25 of water at about room temperature in an atmospheric en-
vironment. The gaseous effluent from said contact com-
prises hydrogen and oxygen and burns when subjected to
electrical sparking. The volume of gas evolved is de-
pendent on reactor block surface area and the volume of
30 water impinging thereon. Generally a 2.5 square cm sur-
face will react with 0.10 gallons of water per minute.

Although the invention has been described in detail
with respect to specific examples, it will be appreciated
that various changes and modifications can be made by
35 those skilled in the art within the scope of the invention
as expressed in the following claims.

The invention having been described, what is claimed is:

1. A material for the generation of hydrogen and oxygen from water which comprises a reactive alloy of an alkali metal and aluminum wherein the atomic ratio of alkali metal to aluminum is from about 1:3 to about 3:1 combined with a catalytic alloy of a metal selected from the platinum metals family or nickel and at least one element selected from the group consisting of germanium, antimony, gallium, thallium, indium and bismuth.
2. The material of Claim 1 further characterized in that the alkali metal is sodium or potassium.
3. The material of Claim 1 further characterized in that the alloy contains antimony.
4. The material of Claim 1 further characterized in that the alloy contains germanium.
5. The material of Claim 1 further characterized in that the alloy also contains a metal selected from the group consisting of zirconium, chromium and mixtures thereof.

6. The material of Claim 1 further characterized
in that the alloy also contains a metal selected from
the group consisting of bismuth, gold and mixtures
4 thereof.

1 7. The material of Claim 1 further comprising tin.

8. The material of Claim 1 further characterized
in that the ratio, by weight, of catalytic alloy to re-
3 active alloy is from about 1:1 to about 1:5.

9. The material of Claim 8 further characterized
in that the ratio, by weight, of catalytic alloy to re-
3 active alloy is about 1:1 to about 1:3.

10. The material of Claim 5 further characterized
in that the catalytic alloy contains from about 0.7% to
3 about 1.1% by weight chromium.

11. The material of Claim 1 further characterized
in that the each of the metallic components of the cata-
lytic alloy present in said material is present in an
amount of from about 0.4 to about 28.5 weight percent
5 based upon the weight of catalytic alloy and reactive
alloy combined.

12. The material of Claim 1 further characterized
in that said catalytic alloy comprises a metal selected
from the platinum metal family present in an amount of
from about 0.4 to about 2.3% by weight, bismuth present
5 in an amount of from about 42.9 to about 71.5% by weight,
antimony present in an amount of from about 25.5 to about
42.5% by weight, chromium present in an amount of from
about 0.7 to about 1.1% by weight, zirconium present in
an amount of from about 4.1 to about 6.8% by weight and
10 gold present in an amount of from about 0.6 to about 2.3%
by weight.

13. The material of Claim 12 further characterized in that said alloy comprises about 1.4 wt. % of platinum, about 57.3 wt. % bismuth, about 34.0 wt. % antimony, about 0.9 wt. % chromium, about 5.4 wt. % zirconium and
5 about 1.0 wt. % gold.

14. A process for the generation of hydrogen and oxygen from water which comprises contacting water with a reactive alloy of an alkali metal and mercury wherein the atomic weight ratio of alkali metal to aluminum is
5 from about 1:3 to about 3:1 combined with a catalytic alloy containing a metal selected from the platinum metal family or nickel.

15. The process of Claim 14 further characterized in that the alkali metal is sodium, potassium or mixtures
3 thereof.

16. The process of Claim 14 further characterized in that the catalytic alloy comprises at least one metal selected from the group consisting of germanium, anti-
4 mony, gallium, thallium, indium and bismuth.

17. The process of Claim 14 further characterized in that the catalytic alloy comprises at least one metal selected from the group consisting of germanium, antimony, gallium, thallium, indium and bismuth and the
5 alkali metal is sodium.

18. The process of Claim 17 further characterized
2 in that the alloy contains antimony.

19. The process of Claim 17 further characterized
2 in that the alloy contains germanium.

20. The process of Claim 17 further characterized in that the alloy also contains a metal selected from the group consisting of zirconium, chromium and mixtures thereof.

21. The process of Claim 17 further characterized in that the alloy also contains a metal selected from the group consisting of bismuth, gold and mixtures thereof.

22. The process of Claim 17 further comprising tin.

23. The process of Claim 17 further characterized in that the ratio by weight, of catalytic alloy to reactive alloy is from about 1:1 to about 1:5.

24. The process of Claim 23 further characterized in that the ratio, by weight, of catalytic alloy to reactive alloy is about 1:1 to about 1:3.

25. The process of Claim 20 further characterized in that the catalytic alloy contains from about 0.7% to about 1.1% by weight chromium.

26. The process of Claim 17 further characterized in that each of the metallic components of the catalytic alloy present in said material is present in an amount of from about 0.4 to about 28.5 weight percent based upon the weight of catalytic alloy and reactive alloy combined.



27. The process of Claim 14 further characterized in that said catalytic alloy comprises a metal selected from the platinum metal family present in an amount of from about 0.4 to about 2.3% by weight, bismuth present in an amount of from about 42.9 to about 71.5% by weight, antimony present in an amount of from about 25.5 to about 42.5% by weight, chromium present in an amount of from about 0.7 to about 1.1% by weight, zirconium present in an amount of from about 4.1 to about 6.8% by weight and gold present in an amount of from about 0.6 to about 2.3% by weight.

28. The process of Claim 27 further characterized in that said alloy comprises about 1.4 wt. % of platinum, about 57.3 wt. % bismuth, about 34.0 wt. % antimony, about 0.9 wt. % chromium, about 5.4 wt. % zirconium and about 1.0 wt. % gold.

INTERNATIONAL SEARCH REPORT

International Application No PCT/US 81/00039

I. CLASSIFICATION OF SUBJECT MATTER (If several classification symbols apply, indicate all) *

According to International Patent Classification (IPC) or to both National Classification and IPC

INT. CL.³ C01B 13/02; C22C 7/00, 30/00
US. CL. 75/134N; 423/579, 657

II. FIELDS SEARCHED

Minimum Documentation Searched *

Classification System	Classification Symbols
US	423/579, 648R, 657 75/134A, 134F, 134N, 134R, 138, 169, 172R

Documentation Searched other than Minimum Documentation
to the Extent that such Documents are Included in the Fields Searched *

III. DOCUMENTS CONSIDERED TO BE RELEVANT ¹⁴

Category *	Citation of Document, ¹⁵ with indication, where appropriate, of the relevant passages ¹⁷	Relevant to Claim No. ¹⁸
A	US, A, 909,536, Published, 12 January 1909, Brindley	1-28
A	US, A, 934,036, Published, 14 September 1909, Brindley	1-28
A	US, A, 3,786,139, Published, 15 January 1974, MacKenzie et al.	1-28
A	US, A, 3,985,866, Published, 12 October 1976, Oda et al	1-28
P	US, A, 4,182,748, Published, 08 January 1980 Anderson	1-28
P	US, A, 4,207,095, Published, 10 June 1980 Anderson	1-28
A	GB, A, 3188, Published, 30 September 1909	1-28
X	WO, A, WO-79/01031, Published, 29 November 1979, Anderson	1-28

* Special categories of cited documents: ¹⁶

"A" document defining the general state of the art

"E" earlier document but published on or after the International filing date

"L" document cited for special reason other than those referred to in the other categories

"O" document referring to an oral disclosure, use, exhibition or other means

"P" document published prior to the International filing date but on or after the priority date claimed

"T" later document published on or after the International filing date or priority date and not in conflict with the application, but cited to understand the principle or theory underlying the invention

"X" document of particular relevance

IV. CERTIFICATION

Date of the Actual Completion of the International Search *	Date of Mailing of this International Search Report *
24 MARCH 1981	30 MAR 1981
International Searching Authority *	Signature of Authorized Officer ¹⁹
ISA/US	EDWARD J. MEROS